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## PATENT SPECIFICATION



Application Date: Dec. 29, 1938. No. 37685/38.

523,218

Complete Specification Left: Nov. 28, 1939.

Complete Specification Accepted: July 9, 1940.

#### PROVISIONAL SPECIFICATION

## Improvements in or relating to Optical Objectives

William of

We, Taylor, Taylor & Hobson Limited, a Company registered under the Laws of Great Britain, and Arthur Warmisham, British Subject, both of 104, Stoughton Street, Leicester, do hereby declare the nature of this invention to be as follows:—

This invention relates to an optical objective for kinematograph projection or other purposes consisting of a lens system corrected for spherical aberration, coma, astigmatism and distortion, of the kind comprising a double-concave asymmetrical divergent component disposed behind two convergent components and in front of a third convergent component and having its shallow side turned towards the front two components, each of the four components being in the form 20 of a simple element, i.e. consisting of a single piece of glass. It should be made clear that the side of the longer conjugate is herein regarded as the "front" of the objective in accordance with the normal 25 convention.

The present applicants' British Patent Application No. 22153 of 1938 (Serial No. 517,386) relates to an objective of this kind, giving for an aperture of, say, F/2 a much higher degree of correction (more especially for curvature of field and coma) over a semi-field of about ten degrees than had previously been obtained. In such objective the glass of the divergent component has its mean refractive index  $n_D$  substantially greater than 1.65 and its Abbé V number substantially less than 33.5 and the air separation on the axis between the 40 shallow side of the divergent component and the convergent component in front of it is not less than 10% of the focal length of the objective, the mean refractive indices of at least two of the three con-45 vergent components preferably being greater than 1.6.

The present invention has for its object

still further to improve the correction in such an objective.

According to the invention the mean 50 refractive indices of at least two of the three simple convergent components are greater than 1.75, whilst that of the divergent component is greater than 1.8. Various examples of glass having such 55 high refractive index are given in British Patent Specification No. 462,304, such glass having as its main constituents oxides of elements such as tungsten, tantalum, lanthanum, thorium, yttrium, 60 zirconium, hafnium and columbium.

Conveniently the sum of the numerical values of the radii of the front surface of the front component and the rear surface of the rear component is greater than 65 1.25 and less than 2.5 times the equivalent focal length of the whole objective.

The numerical value of the radius of

The numerical value of the radius of the front surface of the divergent component is preferably greater than that of 70 the rear surface of the rear convergent component, but both surfaces being concave towards the front. The radius of the rear surface of the rear component is preferably less than 1.75 times the 75 equivalent focal length of the whole objective.

Numerical data for two convenient practical examples of objective according to the invention are given in the following tables, in which the radii of curvature of the individual surfaces are designated by  $R_1$   $R_2$  ... counting from the front, the positive sign indicating that the surface is convex towards the front and the negative sign that it is concave thereto, whilst the thicknesses of the individual elements along the axis are designated by  $D_1$   $D_2$  ..., and the axial air spaces between the various components by  $S_1$   $S_2$   $S_3$ . The tables also give the mean refractive indices and the Abbé V numbers of the glasses used for the individual elements.

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		EXAMPLE	I	
	Equivalent focal length 1.000.		Relative Aperture F/1.8.	
-	Radius	Thickness or Separation	Refractive Index $n_{ exttt{D}}$	Abbé V Number
5	$R_1 + .8521$ $R_2 + 1.1628$	D <sub>1</sub> .1124	1.850	42.0
)	$R_{s} + .5486$	$S_1$ .0068 $D_2$ .1124	1.850	42.0
	$ m R_4 + 1.190 \\  m R_5 - 1.882 $	$S_2$ .1514 $D_3$ .0264	2.022	19.1
5	$R_6 + .4209$ $R_7 + 1.028$	$S_3$ .1329	-	
	•	$D_4$ .0879	1.848	32.5
	$R_{s}$ 6288			
 0	R <sub>8</sub> 6288	Example I		
 )	R <sub>s</sub> 6288  Equivalent focal	-	I. Relative Aper	ture F/2.0.
)		-		ture F/2.0. Abbé V Number
-	Equivalent focal Radius R <sub>1</sub> + .7679	length 1.000. Thickness or	Relative Aper Refractive	Abbé V
-	Equivalent focal	length 1.000.  Thickness or Separation  D <sub>1</sub> .1011 S <sub>1</sub> .0030	Relative Aper Refractive Index $n_p$	Abbé V Number 38.4
-	Equivalent focal  Radius  R <sub>1</sub> + .7679  R <sub>2</sub> - 20.226  R <sub>3</sub> + .4695  R <sub>4</sub> + .6409	length 1.000.  Thickness or Separation  D <sub>1</sub> .1011	Relative Aper Refractive Index $n_p$	Abbé V Number
	$\begin{array}{c} {\rm Equivalent\ focal} \\ {\rm Radius} \\ \\ {\rm R}_{\rm I}+  .7679 \\ {\rm R}_{\rm 2}-20.226 \\ {\rm R}_{\rm 3}+  .4695 \end{array}$	D <sub>1</sub> .1011 S <sub>1</sub> .0030 D <sub>2</sub> .0900	Relative Aper Refractive Index $n_p$	Abbé V Number 38.4

Dated this 28th day of December, 1938.

A. F. PULLINGER, Agent for the Applicants.

#### COMPLETE SPECIFICATION

### Improvements in or relating to Optical Objectives

We, Taylor, Taylor & Hobson
40 Limited, a Company registered under the
Laws of Great Britain, and Arthur
Warmisham, British Subject, both of
104, Stoughton Street, Leicester, do
hereby declare the nature of this inven45 tion and in what manner the same is to be
performed, to be particularly described
and ascertained in and by the following
statement:—

This invention relates to an optical objective for kinematograph projection or 50 other purposes consisting of a lens system corrected for spherical aberration, coma, astigmatism and distortion, of the kind comprising a double-concave asymmetrical divergent component disposed 55 behind two convergent components and in front of a third convergent component and having its shallow side turned

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towards the front two components, each of the four components being in the form of a simple element, i.e. consisting of a single piece of glass. It should be made 5 clear that the side of the longer conjugate is herein regarded as the "front" of the objective in accordance with the normal convention.

The present applicants' British Patent Application No. 22153 of 1938 (Serial Number 517,386) relates to an objective of this kind, giving for an aperture of, say, F/2 much higher degree of correction (more especially for curvature of field and coma) over a semi-field of about

15 field and coma) over a semi-field of about ten degrees than had previously been obtained. In such objective the glass of the divergent component has its mean refractive index  $n_{\text{D}}$  substantially greater

20 than 1.65 and its Abbé V number substantially less than 33.5 and the air separation on the axis between the shallow side of the divergent component and the convergent component in front of it is not 25 less than 10% of the focal length of the

objective, the mean refractive indices of at least two of the three convergent components preferably being greater than 1.6.

The present invention has for its object

30 still further to improve the correction in

such an objective.

According to the invention the mean refractive indices of at least two of the three simple convergent components are 35 greater than 1.75, whilst that of the divergent component is greater than 1.8. Various examples of glass having such high refractive index are given in British Patent Specification No. 462,304, such

glass having as its main constituents 40 oxides of elements such as tungsten, tantalum, lanthanum, thorium, yttrium, zirconium, hafnium and columbium.

Conveniently the sum of the numerical values of the radii of the front surface of 45 the front component and the rear surface of the rear component is greater than 1.25 and less than 2.5 times the equivalent focal length of the whole objective.

The numerical value of the radius of 50 the front surface of the divergent component is preferably greater than that of the rear surface of the rear convergent component, both such surfaces being concave towards the front. The radius of 55 the rear surface of the rear component is preferably less than 1.75 times the equivalent focal length of the whole objective.

Numerical data for three convenient 60 practical examples according to the invention (of which the first is illustrated in the accompanying drawing) are given in the following tables, in which the radii of curvature of the individual surfaces are designated by  $R_1$ ,  $R_2$ ... counting from the front, the positive sign indicating that the surface is convex towards the front and the negative sign that it is concave thereto, whilst the thicknesses of the individual elements along the axis are designated by  $D_1$ ,  $D_2$ ..., and the axial air spaces between the various components by  $S_1$ ,  $S_2$ ,  $S_3$ . The tables also give the mean refractive indices and the 75 Abbé V numbers of the glasses used for the individual elements.

EXAMPLE I.

	Equivalent focal length 1.000.		Relative Aperture F/1.8.	
80	Radius	Thickness or Separation	Refractive Index $n_{\rm p}$	Abbé V Number
	$R_1 + .8521$	70		<del></del>
	$R_2 + 1.1628$	$D_1$ .1124	1.850	42.0
85	$R_{a} + .5486$	S <sub>1</sub> .0068		
	$R_4 + 1.190$	D <sub>2</sub> .1124	1.850	42.0
90	_	$S_2$ .1514	•	·
	$R_s = 1.882$	$\mathbf{D}_{\mathfrak{s}}$ .0264	2.022	19.1
	$R_{6} + .4209$	S <sub>3</sub> .1329		
95	$R_7 + 1.028$	$\mathbf{D}_{4}$ .0879	1.848	90 ¤
	$R_{s}$ - $.6288$	104 .0010	1.040	32.5

EXAMPLE II.

	Equivalent focal length 1.000.		Relative Aperture F/2.0.	
	${f Radius}$	Thickness or Separation	$\begin{array}{c} \text{Refractive} \\ \text{Index,}  n_{\mathtt{p}} \end{array}$	Abbé V Number
5	R <sub>1</sub> + .7679	D <sub>1</sub> .1011	1.800	38.4
10	$ m R_{2} - 20.226 \  m R_{3}4695 \  m$	S <sub>1</sub> .0030	1 000	90.4
10	$R_4 + .6409$	$D_2$ .0900 $S_2$ . 0870	1.800	38.4
15	$ m R_{s} - 15.807$ $ m R_{6} + .4103$	D <sub>3</sub> .0243	2.022	19.1
	$R_{\tau} + 1.686$	$egin{array}{ccc} S_3 & .3034 \ D_4 & .0566 \ \end{array}$	1.842	35.5
	$R_s$ – $.8015$			

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EXAMPLE III.

	Equivalent focal length 1.000.		Relative Aperture F/2.0.	
	Radius	Thickness or Separation	$\begin{array}{c} \text{Refractive} \\ \text{Index} \ n_{\scriptscriptstyle \mathrm{D}} \end{array}$	Abbé V Number
25	$R_1 + .7653$ $R_2 - 11.35$	D1007	1.800	38.4
30	$R_a + .4062$ $R_4 + .5767$	$S_1$ .0029 $D_2$ .0854	1.613	37.3
90	$R_{5} - 8.796$	$S_2 = .0867$ $D_3 = .0247$	2.022	19.1
<u>35</u>	$ m R_{r} + \ .3929$ $ m R_{r} + \ 1.574$	S <sub>3</sub> .2829		
	$\mathbf{R_{s}}$ 7651	D <sub>4</sub> .0564	1.842	<b>3</b> 5.5

It will be noticed that in Examples I 40 and II all three convergent elements are made of glass having a mean refractive index  $n_D$  greater than 1.75, whilst in Example III two only of such elements are of the high index glass. The sum of

45 the numerical values of the radii R<sub>1</sub> and R<sub>8</sub> is 1.4809 in Example I, 1.5694 in Example II and 1.5304 in Example III. In each example the fifth and eighth sur-

faces are both concave to the front and 50 the radius R<sub>s</sub> is much greater than the radius R<sub>s</sub>, the radius R<sub>s</sub> being numerically less than 1.75.

Having now particularly described and ascertained the nature of our said invention and in what manner the same is to be 55 performed, we declare that what we claim

1. An optical objective of the kind described, in which the mean refractive indices of at least two of the three simple 60 convergent components are greater than 1.75, whilst that of the divergent component is greater than 1.8.

2. An objective as claimed in Claim 1, in which the sum of the numerical values 65 of the radii of the front surface of the front component and the rear surface of the rear component is greater than 1.25 and less than 2.5 times the equivalent focal length of the whole objective.

3. An objective as claimed in Claim 1 or Claim 2, in which the numerical value of the radius of the front surface of the divergent component is greater than that of the rear surface of the rear convergent component, both such surfaces being concave towards the front.

4. An objective as claimed in Claim 1 or Claim 2 or Claim 3, in which the

radius of the rear surface of the rear com- 10 ponent is less than 1.75 times the equivalent focal length of the whole objective.

5. An objective having numerical data substantially as set forth in any one of the tables herein.

Dated this 28th day of November, 1939.

PULLINGER & MALET-VEALE,

Agents for the Applicants.

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